



The computation of bending eigenfrequencies of single-walled carbon nanotubes based on the nonlocal theory

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Abstract. In this work, a recently proposed nonlocal theory of bending is used in the analysis of eigenfrequencies of single-walled carbon nanotubes (SWCNTs). The nanotube vibration is analyzed in the form of a homogenized continuum. Classical treatment where a nanotube is approximated by standard beam theory, is replaced by the more sophisticated nonlocal method of material interactions where a nonlocal parameter is used. The eigenfrequencies are computed by the combination of analytical as well as numerical methods for four different carbon nanotube (CNT) supports. Various types of supports are considered for the analysis: fixed–simply supported, fixed–free, simply–simply supported and fixed–fixed. Due to the huge amount of computed data, only outcomes of eigenfrequency computations for the nanobeams of armchair type with fixed and simply supported ends, and different nonlocal parameters are represented in the form of graphs at the end of the article. The study shows how the nanotube eigenfrequencies depend on nonlocal parameters as well as on the length and diameter of CNTs. The obtained results are in good agreement with the results published in papers which were gained by different procedures.

1 Introduction

Functional materials and nanomaterials are attracting a lot of attention in the areas of modern engineering. The internal structure of such materials is relatively simple but the determination of their properties is often associated with difficulties. In many cases, the theoretical treatments with indirect measurements of conjugated behavior lead to the solution of a stated problem. In our case, we will deal with the determination of eigenfrequencies of carbon nanotubes. The eigenfrequencies are very important parameters of these structures because their measurement can serve as a base for the determination of elastic properties, e.g., Young's modulus of homogenized materials.

The massive investigation of carbon nanotubes started after publishing well-known article (Iijima, 1991). CNTs are large macromolecules composed exclusively of carbon atoms. Nanotubes can be formally obtained by rolling up a single-walled plane sheet of graphite, called graphene, into

a cylindrical shape. Nanotubes have remarkable mechanical properties. The most important task in the design of a machine is to find an adequate material for a particular structure. In principle, the aim is to use strength and lightweight material. Nowadays, in mechanical engineering, the carbon nanotubes are candidates that fulfill such demands as parts of composite materials (Wu and Chou, 2012; Yayli, 2014). Besides of mechanical properties, the scientists focus their research on electrical, thermal and optical properties of CNTs. Many applications of CNTs are oriented to the area of biology and medicine.

Depending on the scale, the simulation of SWCNTs is realized by several methods: atomistic scale simulation, simulation by molecular dynamic and the macroscale continuum treatment. In this paper, the third method is applied to describe the bending eigenfrequencies of CNTs. As the elements of nanostructure have special properties, the homogenized continuum of CNTs has to reflect such specific behavior. The standard theory of elasticity is built on the principle

of local action, i.e. the response at a point depends on actions in its neighborhood. However, this is not the case of nanostructures. Here, nonlocal influences can occur and therefore, the nonlocal theory has to be used (Eringen, 2002). According to the underlying theory, strain in every point of a body influences a stress level at the investigated point.

Different applications of the nonlocal theory can be found in many research papers. A review on the application of the nonlocal continuum theory for static and dynamic loadings of carbon nanotubes and graphene sheets is presented in the paper of Arash and Wang (2012). The nonlocal elastic beam model, the elastic shell model and the elastic plate model is established for modeling carbon nanotubes and graphene sheets. The different loading states as bending under transverse loading of CNTs, buckling analysis of axial loaded CNTs and free vibration of CNTs are described. Using the nonlocal continuum mechanics in nonlinear stability analysis of graphene sheets is presented in paper (Asemi et al., 2014). The Galerkin method with the nonlocal parameter for the analysis of simply supported orthotropic graphene sheets is used. The paper reports that the nonlocal parameter has significant effect on the postbuckling behavior of graphene sheets. Kirchhoff's plate theory with the nonlocal parameter is used for eigenfrequency investigation of nanoplates with elastic (Winkler–Pasternak) boundary conditions in the research of Chakraverty and Behera (2015). The effect of the aspect ratio, the elastic boundary conditions and the nonlocal parameter is presented. A forced vibration of a single- and double-walled carbon nanotube under excitation of a moving harmonic load has been analyzed using nonlocal elasticity theory by Rahmani et al. (2017, 2018).

The vibrations of tensioned nanobeams using the nonlocal beam theory are investigated by Bagdatli (2015). The nonlinear frequencies for fixed–fixed and simply–simply supported Euler–Bernoulli nanobeams are presented. The vibration behavior of the nanobeams with small scale effects represented by the nonlocal parameter is studied in the research of Lim et al. (2010). The forced vibration of SWCNTs is investigated by the nonlocal theory in Şimşek (2010). The SWCNTs as nonlocal Euler–Bernoulli beams are modeled and the effects of aspect ratio and nonlocal parameter on vibration behavior of SWCNTs are discussed. The vibrational behavior of CNTs using wave propagation approach is studied by Hussain et al. (2017), Hussain and Nawaz (2017). Other applications of the nonlocal theory and the vibration behavior of carbon nanotubes with different boundary conditions can be found in papers (Narendar and Gopalakrishnan, 2012; Şimşek, 2011; Thongyothee et al., 2013; Wang et al., 2015; Yang et al., 2010). The properties of single-walled carbon nanotubes are well described in papers (Arash and Wang, 2012; Fu et al., 2012; Gupta and Batra, 2008; Harik, 2002; Karličić et al., 2015; Kumar and Srivastava, 2016; Lee and Chang, 2012).

In this paper, the bending frequencies of single-walled carbon nanotubes based on nonlocal stress theory are investigated. The carbon nanotubes are represented by the Euler–

Bernoulli nanobeams with nonlocal parameter. The authors previously published bending eigenfrequencies for different types of boundary conditions and chirality (and corresponding diameters) in papers Bocko and Lengvarský (2014a, b, c). Novelty of paper lies in investigation of chirality effects to eigenfrequencies, comparison of semianalytical methods with the finite element method (FEM) for different nonlocal parameters for boundary condition of type fixed–free. Further, the eigenfrequencies are computed for four different supports (fixed–simply supported, fixed–free, simply–simply supported and fixed–fixed) of carbon nanotubes, the semianalytical results for fixed–simply supported armchair CNTs with different lengths and five nonlocal parameters are presented in graphical form at the end of the article. Finally, the comparison of the results with results from Imani Yengejeh et al. (2014), Lü et al. (2007), Zhang et al. (2009) is done.

2 Carbon nanotube as a beam

The elasticity theory of continuum media is based on several fundamental assumptions: the principle of objectivity, determinism, material symmetry, equipresence, causality, local action, etc. The principle of local action represents the fact that stress at a material point is related exclusively to the deformations in its immediate surroundings. On the other hand, in the nonlocal continuum theory, this assumption is abandoned, and the stress tensor at the investigated part of continua is influenced by the movement of all points of continua (Eringen, 2002). The equation for nonlocal stress is written as:

$$\sigma(\mathbf{x}) = \int_V \mathbf{K}(|\mathbf{x}' - \mathbf{x}|, \tau) \mathbf{T}(\mathbf{x}') dV(\mathbf{x}'), \quad (1)$$

$$\mathbf{T}(\mathbf{x}) = \mathbf{C}(\mathbf{x}) : \boldsymbol{\epsilon}(\mathbf{x}). \quad (2)$$

Here, $\mathbf{T}(\mathbf{x})$ is the stress tensor at point \mathbf{x} , $\mathbf{C}(\mathbf{x})$ is the fourth-order elasticity tensor, $\boldsymbol{\epsilon}(\mathbf{x})$ is the strain tensor and relation $\mathbf{K}(|\mathbf{x}' - \mathbf{x}|, \tau)$ is the nonlocal modulus defined by Eringen (2002). The material parameter τ is expressed by relation $\tau = \sqrt{\mu}/l$. Here, the so-called nonlocal parameter μ represents the influence of using very small distances. This parameter can be evaluated from relation $\mu = e_0^2 l_i^2$. Here, e_0 is a material constant, l_i is the internal characteristic length and l is the external characteristic length. More information about using the nonlocal parameter μ in connection with beams can be found in Reddy and Pang (2008). Simplified Eq. (1) can be written as:

$$(1 - \tau^2 l^2 \nabla^2) \sigma = \mathbf{T}, \quad (3)$$

where ∇^2 is the Laplacian operator. The theory of homogeneous isotropic beam, together with above-mentioned premise, results in the equation relating normal strain ϵ_{xx} and normal stress σ_{xx} by Young's modulus E and parame-

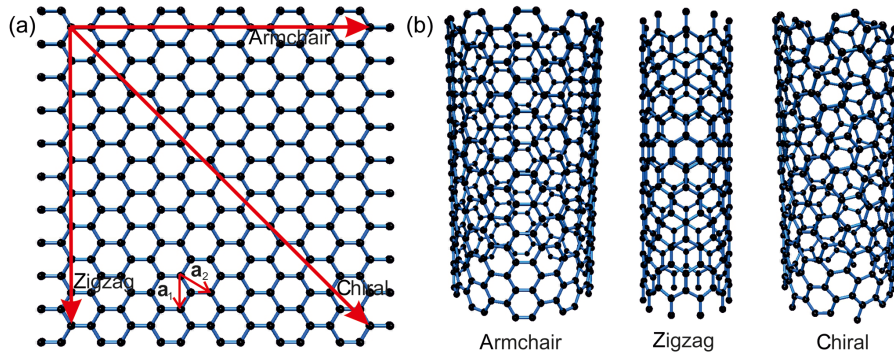


Figure 1. The scheme of lattice structures (a) graphene sheet, (b) single-walled carbon nanotubes.

ter μ (Thongyothee et al., 2013):

$$\sigma_{xx} - \mu \frac{\partial^2 \sigma_{xx}}{\partial x^2} = E \varepsilon_{xx}. \tag{4}$$

Combination of the nonlocal theory and the theory of free vibration of a beam allows us to write the following relation (Thongyothee et al., 2013):

$$m_b(x)\mu \frac{\partial^2 u}{\partial t^2} + \frac{\partial^2}{\partial x^2} \left[EJ(x) \frac{\partial^2 u}{\partial x^2} \right] = 0. \tag{5}$$

Here, u is the transverse displacement of the beam, m_b is the mass of beam related to the unit length, J is the second moment of cross-section area. In the overall motions of the beam, the various parts will move in unison, the relative proportion of their displacements being unchanged with time. This leads to the separation of space and time variables. Finally, considering constant cross-section of the beam, we get the differential equation of fourth order with respect to the independent space variable x :

$$\psi^{IV}(x) - \beta^4 \psi(x) = 0. \tag{6}$$

Here, $\psi(x)$ is an eigenvector (eigenmode) and the parameter β is defined as:

$$\beta^4 = \frac{\omega^2 \mu m_b}{EJ} \tag{7}$$

The scalar quantity ω , in the above relation, is the angular frequency of vibrations of the free CNT. The substitution of β into the Eq. (6), results into the formula:

$$\psi(x) = B_1 \cos(\beta x) + B_2 \cosh(\beta x) + B_3 \sin(\beta x) + B_4 \sinh(\beta x) \tag{8}$$

Here, B_1, B_2, B_3, B_4 are determined in accordance with the given support conditions of the nanobeam.

3 The Numerical solution of frequency equation

3.1 Geometry of carbon nanotubes

Rolling up of a graphene sheet (Fig. 1a) can be accomplished in many ways and in principle it can be described by a chiral

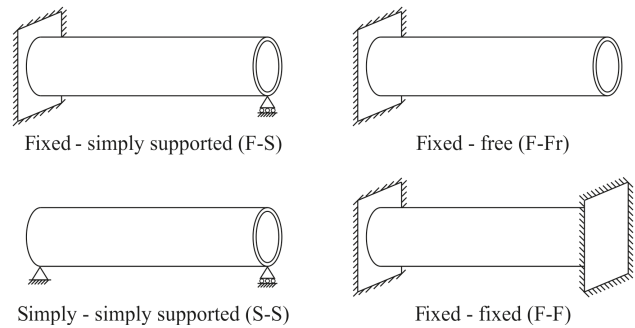


Figure 2. The applied boundary conditions on nanobeams.

vector c_h or a chiral angle θ :

$$c_h = n a_1 + m a_2, \tag{9}$$

$$\theta = \arcsin \frac{\sqrt{3}m}{2\sqrt{n^2 + m^2 + nm}}. \tag{10}$$

Having fixed vectors a_1 and a_2 the pairs of integers (n, m) specify the chirality of SWCNT. Two limit states of CNTs $(n, 0)$ or $(\theta = 0^\circ)$ and (n, n) or $(\theta = 30^\circ)$ are called zigzag and armchair (Fig. 1b), respectively. The intermediate states of CNTs (n, m) or $(0^\circ < \theta < 30^\circ)$ define chiral nanotubes, (Fig. 1b).

Chirality influences the response of carbon nanotubes to external disturbances. Beside of chirality we will use another important characteristic parameter of the carbon nanotube, its length L .

3.2 Boundary conditions

In this paper we have focused our attention on the CNTs with the following types of boundary conditions (Fig. 2): fixed–simply supported (F–S), fixed–free (F–Fr), simply–simply supported (S–S) and fixed–fixed (F–F).

3.3 Semianalytical solution

The application of boundary conditions to the differential equation results in the following characteristic equations:

$$(F-S) : \begin{vmatrix} \sin(\beta L) & \cosh(\beta L) \\ \sin(\beta L) + \sinh(\beta L) & \cos(\beta L) + \cosh(\beta L) \end{vmatrix} = 0, \quad (11)$$

$$(F-Fr) : \begin{vmatrix} \sin(\beta L) + \sinh(\beta L) & \cos(\beta L) + \cosh(\beta L) \\ \cos(\beta L) + \cosh(\beta L) & \sinh(\beta L) - \sin(\beta L) \end{vmatrix} = 0, \quad (12)$$

$$(S-S) : \begin{vmatrix} \sin(\beta L) & \sinh(\beta L) \\ -\sin(\beta L) & \sinh(\beta L) \end{vmatrix} = 0, \quad (13)$$

$$(F-F) : \begin{vmatrix} \sin(\beta L) - \sinh(\beta L) & \cos(\beta L) - \cosh(\beta L) \\ \cos(\beta L) - \cosh(\beta L) & -\sin(\beta L) - \sinh(\beta L) \end{vmatrix} = 0, \quad (14)$$

and they finally lead to the relations:

$$(F-S) : \sinh(\beta L) \cos(\beta L) - \cosh(\beta L) \sin(\beta L) = 0, \quad (15)$$

$$(F-Fr) : 1 + \cos(\beta L) \cosh(\beta L) = 0, \quad (16)$$

$$(S-S) : \sin(\beta L) \sinh(\beta L) = 0, \quad (17)$$

$$(F-F) : -1 + \cos(\beta L) \cosh(\beta L) = 0. \quad (18)$$

Because the nanotube is modeled as a continuum by homogenization method, the characteristic equations are transcendental ones. The roots (βL) of the equations for the prescribed supports were obtained using program MATLAB[®]. The first fourth values (βL) can be found in Table 1. The radian frequencies ω result from Eq. (7) and for the frequencies f we have formula $f = \omega/2\pi$.

The second moment of area J with respect to the axis which is perpendicular to the axial direction of the beam is related to the thickness of the nanotube shell. Because there is no certainty in the definition of this parameter, different values can be found in the literature. Here, we use relations from Swain et al. (2013):

$$m_b = \rho A = 4.8 \times 10^{-24} R \quad (\text{kg nm}^{-1}), \quad (19)$$

$$EJ = 1713.92R^2 - 794.16R + 109.24 \quad (\text{kg nm}^{-3} \text{s}^{-2}), \quad (20)$$

where R is the radius of the nanotube. The chirality parameters (n, m) characterize the radius of CNT, and the radius is defined by equation:

$$R = a_0 \sqrt{3(n^2 + m^2 + nm)}/2\pi \quad (21)$$

where $a_0 = 0.1424$ nm is the distance between two neighboring carbon atoms and the chirality parameters for our computations are $m = n$.

4 Finite element modelling of carbon nanotubes

In this chapter, the nonlocal finite element formulation is presented. The mass and stiffness matrices of finite element are derived from Eq. (5).

The element stiffness matrix can be defined as:

$$\mathbf{K}_e = EJ \int_0^{l_e} \frac{d^2 \mathbf{N}(x)}{dx^2} \frac{d^2 \mathbf{N}^T(x)}{dx^2} dx \quad (22)$$

Table 1. Solutions of frequency equations for different boundary conditions.

Eigenfrequency no.	Value of (βL)			
	F-S	F-Fr	S-S	F-F
1	3.9266	1.8751	3.1415	4.7300
2.	7.0685	4.6940	6.2831	7.8532
3.	10.2101	7.85475	9.4247	10.9956
4.	13.3517	10.9955	12.5663	14.1371

$$= \frac{EJ}{l_e^3} \begin{bmatrix} 12 & 6l_e & -12 & 6l_e \\ 6l_e & 4l_e^2 & -6l_e & 2l_e^2 \\ -12 & -6l_e & -12 & -6l_e \\ 6l_e & 2l_e^2 & -6l_e & 4l_e^2 \end{bmatrix}$$

and the nonlocal element mass matrix can be defined as:

$$\mathbf{M}_e = m_b \mu \int_0^{l_e} \frac{d^2 \mathbf{N}(x)}{dx^2} \frac{d^2 \mathbf{N}^T(x)}{dx^2} dx \quad (23)$$

$$= \frac{m_b \mu l_e}{420} \begin{bmatrix} 156 & 22l_e & 54 & -13l_e \\ 22l_e & 4l_e^2 & 13l_e & -3l_e^2 \\ 54 & 13l_e & 156 & -22l_e \\ -13l_e & -3l_e^2 & -22l_e & 4l_e^2 \end{bmatrix}$$

5 Results and discussion

At first, the effect of chirality on the eigenfrequencies of CNTs is investigated. The chirality angle varies from 0 to 30°. The semianalytical computations of the first two eigenfrequencies are accomplished for different types of CNTs but with approximately the same diameters. The length of the tubes is 10 nm and the following types of boundary conditions are used (Fig. 2): fixed-free (F-Fr) and simply-simply supported (S-S). From computations (Table 2) result that the chirality has effect on the change of CNTs eigenfrequencies due to the small change of tube diameter. The maximum difference in the eigenfrequencies is 7%. Under otherwise identical conditions, the effect of the chirality of SWCNTs can be neglected. For this reason, only armchair CNTs are investigated in this paper.

The results for the tube chirality (5,5), length 10 nm and boundary condition of type F-Fr computed by the semianalytical as well as FEM are given in Table 3. The 100 elements are used for the FEM. It is clear from the results that both methods give almost the same results.

The semianalytical computations for armchair single-walled carbon nanotubes with F-S, F-Fr, S-S and F-F boundary conditions were accomplished in commercial program system MATLAB[®]. The chirality of armchair carbon nanotubes was changed from (4, 4) to (20, 20) which corresponds to the range of diameters from $D = 0.5424$ nm

Table 2. Eigenfrequencies of carbon nanotubes with different chiral angles and boundary conditions.

SWCNT (<i>n, m</i>)	Chiral angle (°)	Diameter (nm)	Frequency (THz)			
			F–Fr (1st)	F–Fr (2nd)	S–S (1st)	S–S (2nd)
(9, 0)	0.00	0.7047	0.02795	0.17515	0.07845	0.31381
(8, 2)	10.89	0.7177	0.02858	0.17912	0.08023	0.32092
(7, 3)	17.00	0.6960	0.02753	0.17249	0.07726	0.30905
(6, 4)	23.41	0.6826	0.02689	0.16852	0.07548	0.30192
(5, 5)	30.00	0.6781	0.02668	0.16719	0.07489	0.29955

Table 3. The first eigenfrequency of carbon nanotubes for both methods with different nonlocal parameter.

	Frequency (THz)					
	$\mu = 0$	$\mu = 0.01$	$\mu = 0.1$	$\mu = 0.4$	$\mu = 1.4$	$\mu = 3$
Semianalytical method	0.02668	0.26679	0.08437	0.04218	0.02255	0.01541
FEM	0.02675	0.26757	0.08461	0.04231	0.02262	0.01545
Error (%)	0.26	0.29	0.28	0.31	0.31	0.26

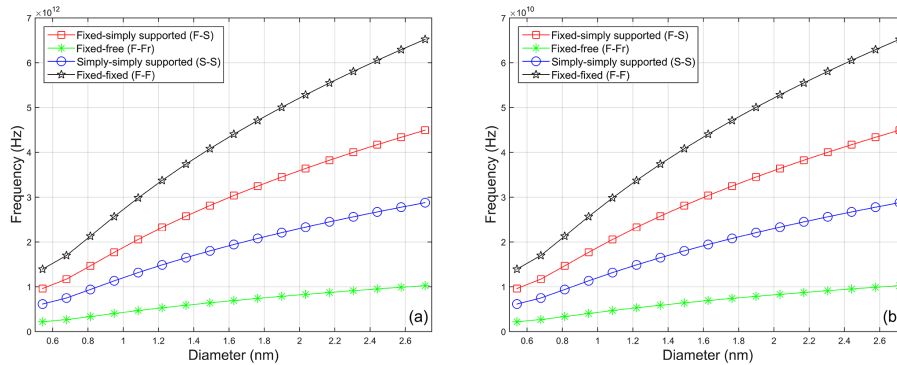


Figure 3. The first eigenfrequencies of armchair nanotubes with the nonlocal parameter $\mu = 0.01$ and length (a) $L = 10$ nm, (b) $L = 100$ nm.

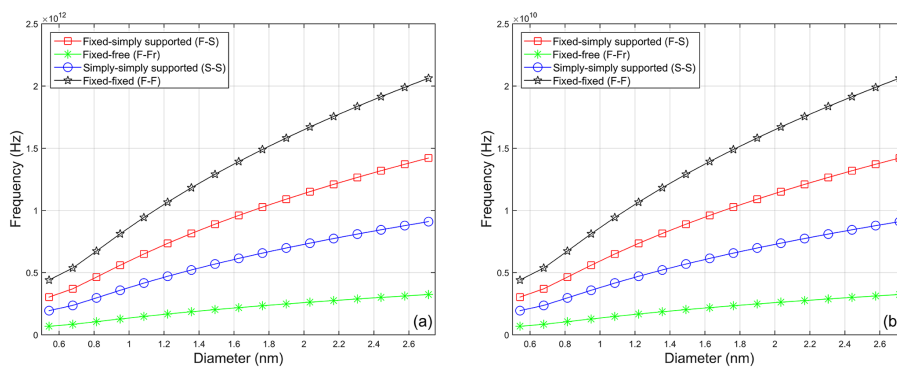


Figure 4. The first eigenfrequencies of armchair nanotubes with the nonlocal parameter $\mu = 0.1$ and length (a) $L = 10$ nm, (b) $L = 100$ nm.

to $D = 2.712$ nm. The length of considered CNTs varies from $L = 10$ nm to $L = 100$ nm. The nonlocal parameter μ is chosen to be 0.01, 0.04, 0.1, 0.3 and 0.4, respectively. The minimal computed eigenfrequency $f = 0.9289$ GHz was obtained for the fixed–free CNT with the diameter $D =$

0.5424 nm, the length $L = 100$ nm and the nonlocal parameter $\mu = 0.4$. The maximal computed eigenfrequency $f = 6.5223$ THz is related to the fixed–free CNT with the diameter $D = 2.712$ nm, the length $L = 10$ nm and the nonlocal parameter $\mu = 0.01$. The dependence of the first eigenfre-

Table 4. The first eigenfrequencies of armchair nanotubes with length $L = 10$ nm for different boundary conditions and nonlocal parameters μ .

Boundary conditions	Diameter (nm)	Frequency (THz)				
		$\mu = 0.01$	$\mu = 0.04$	$\mu = 0.1$	$\mu = 0.3$	$\mu = 0.4$
F–S	1.356	2.5761	1.288	0.8146	0.4703	0.4073
	2.712	4.4948	2.2474	1.4214	0.8206	0.7107
F–Fr	1.356	0.5875	0.2937	0.1858	0.1073	0.0929
	2.712	1.025	0.5125	0.3241	0.1871	0.1621
S–S	1.356	1.649	0.8245	0.5215	0.3011	0.2607
	2.712	2.8772	1.4386	0.9098	0.5253	0.4549
F–F	1.356	3.7381	1.869	1.1821	0.6825	0.5911
	2.712	6.5224	3.2612	2.0626	1.1908	1.033

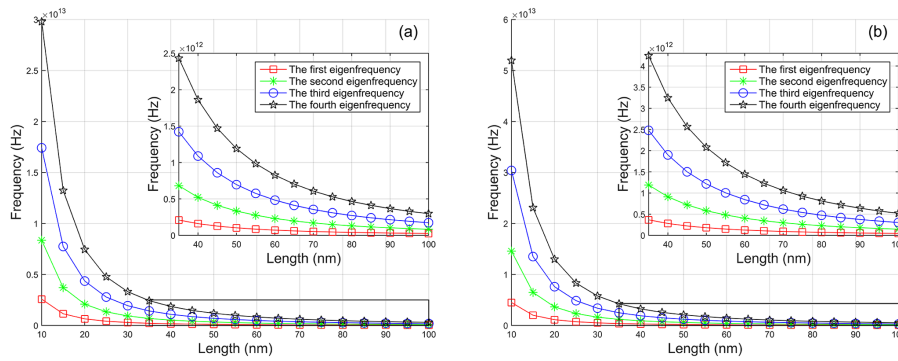


Figure 5. The first four eigenfrequencies of fixed–simply supported armchair nanotubes with nonlocal parameter $\mu = 0.01$, (a) nanotube with chirality $(n, m) = (10, 10)$ and diameter $D = 1.356$ nm, (b) nanotube with and chirality $(n, m) = (20, 20)$, diameter $D = 2.712$ nm.

quencies of armchair SWCNTs with the nonlocal parameter $\mu = 0.01$ on the diameter for 10 nm long CNT is shown in Fig. 3a and for 100 nm in Fig. 3b. Similarly, Fig. 4 shows the results of computations for the nonlocal parameter $\mu = 0.1$, so that the dependence of the first eigenfrequencies of armchair SWCNTs with the nonlocal parameter on the diameter for 10 nm long CNT is shown in Fig. 4a and for 100 nm in Fig. 4b.

The graphs conclude that increasing diameter of the carbon nanotube leads to higher first eigenfrequency and the eigenfrequencies of ten times longer carbon nanotubes are hundred times lower. Comparison of Figs. 3 and 4 shows that ten times higher value of nonlocal parameter leads to approximately three times lower eigenfrequencies. The value of nonlocal parameter affects more the eigenfrequencies of the carbon nanotubes with a smaller diameter.

As there is a huge number of possible combinations of parameters, we have focused our attention on the first eigenfrequencies for the diameters $D = 2R = 1.356$ nm for chirality $(10, 10)$ and $D = 2.712$ nm for chirality $(20, 20)$. The comparison of the first eigenfrequencies for all considered boundary conditions of armchair nanotubes with the length $L = 10$ nm is given in Table 4. It is clear from Table 4 that diameter, nonlocal parameter and boundary conditions have

effect on the eigenfrequencies of nanotubes. In principle, the higher value of the nonlocal parameter the lower value of eigenfrequencies. Opposite tendency is seen for the diameter of CNTs. The highest first eigenfrequencies were computed for the fixed–fixed boundary conditions of CNTs and the lowest first eigenfrequencies for the fixed–free boundary conditions.

Due to complexity, the effect of the nonlocal parameter on only first four eigenfrequencies of armchair CNTs was studied. The graphs in Figs. 5–9 show relations between eigenfrequencies and length L of carbon nanotube with the F–S type boundary conditions. The nonlocal parameter was the same as above.

The graphs show that the eigenfrequencies decrease with increasing length and nonlocal parameter. The eigenfrequencies for the nonlocal parameter equal 0.01 are approximately three times lower than for the nonlocal parameter 0.1.

Because different authors use different parameters for nanotube description in the literature (density, Young’s modulus, nominal thickness of nanotube, boundary conditions), we compared our results only with those where the authors used similar inputs. As a number of such inputs was published for the boundary conditions of type fixed–free, Table 5 gives the comparison of the first eigenfrequencies computed

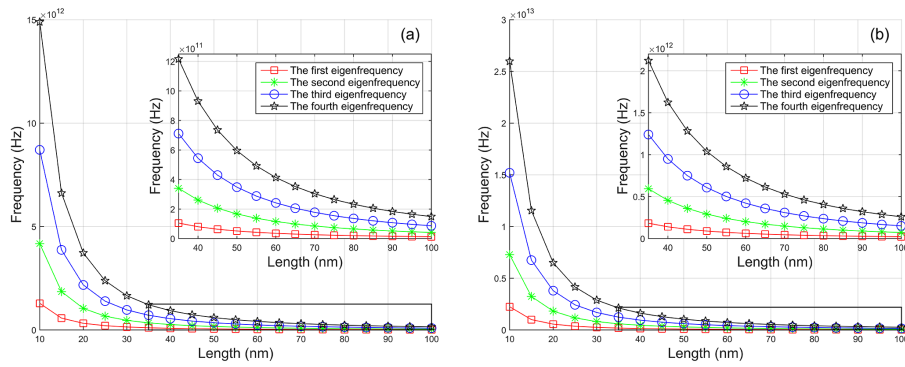


Figure 6. The first four eigenfrequencies of fixed–simply supported armchair nanotubes with nonlocal parameter $\mu = 0.04$, (a) nanotube with chirality $(n, m) = (10, 10)$ and diameter $D = 1.356$ nm, (b) nanotube with and chirality $(n, m) = (20, 20)$, diameter $D = 2.712$ nm.

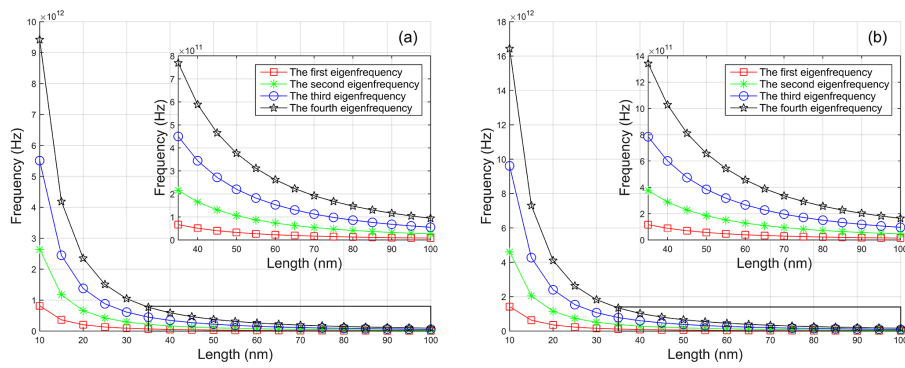


Figure 7. The first four eigenfrequencies of fixed–simply supported armchair nanotubes with nonlocal parameter $\mu = 0.1$, (a) nanotube with chirality $(n, m) = (10, 10)$ and diameter $D = 1.356$ nm, (b) nanotube with and chirality $(n, m) = (20, 20)$, diameter $D = 2.712$ nm.

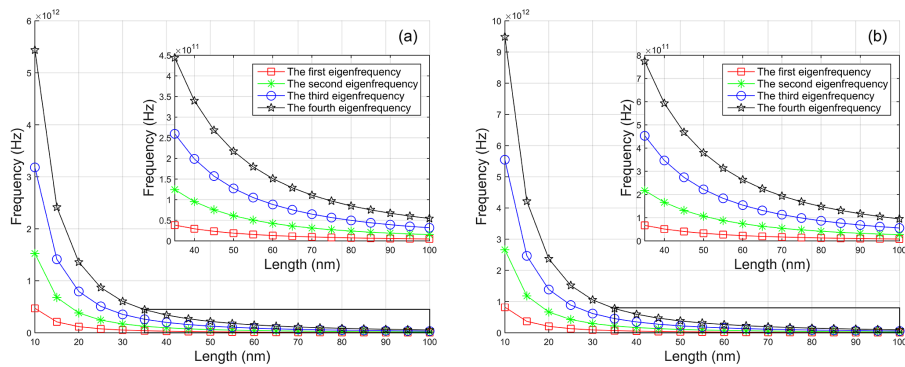


Figure 8. The first four eigenfrequencies of fixed–simply supported armchair nanotubes with nonlocal parameter $\mu = 0.3$, (a) nanotube with chirality $(n, m) = (10, 10)$ and diameter $D = 1.356$ nm, (b) nanotube with and chirality $(n, m) = (20, 20)$, diameter $D = 2.712$ nm.

by different authors and methods with the result of method in the article. The biggest difference in this comparison does not exceed 15 %.

6 Conclusion

We discussed the analytical computation of eigenfrequencies of SWCNTs based on nonlocal beam theory and the numer-

ical results are given for armchair SWCNTs. In the nonlocal theory, the response of a structure at the point of a question is influenced by all particles of the structure. The small scale length effect of the CNTs was represented by the nonlocal parameter in the nonlocal beam theory. The transcendental frequency equations resulting from four different boundary conditions have been solved by computer system MATLAB® and parametric studies of results for the fixed–simply sup-

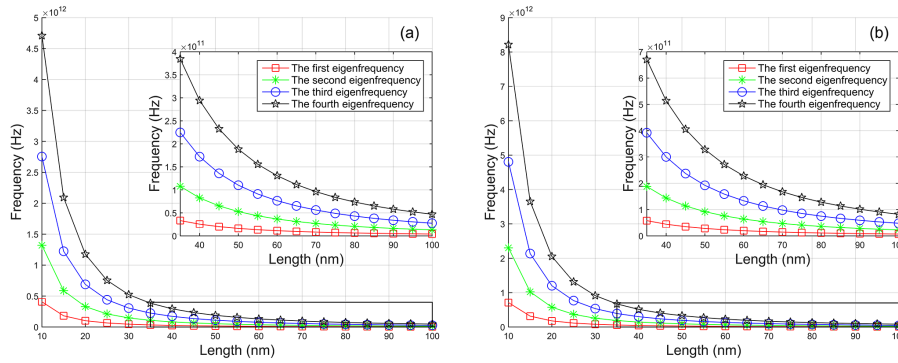


Figure 9. The first four eigenfrequencies of fixed–simply supported armchair nanotubes with nonlocal parameter $\mu = 0.4$, **(a)** nanotube with chirality $(n, m) = (10, 10)$ and diameter $D = 1.356$ nm, **(b)** nanotube with and chirality $(n, m) = (20, 20)$, diameter $D = 2.712$ nm.

Table 5. The comparison of the first eigenfrequencies with published results.

Author	Nanotube chirality	Length (nm)	Method*	Frequency (THz)	Presented method (THz)	Difference (%)
Zhang et al. (2009)	(5, 5)	3.1	MD	0.2319	0.26	-12.12
			LT	0.26357		1.35
			NT $\mu = 1.25$	0.26386	0.248	6.01
	(5, 5)	6.8	MD	0.0549	0.058	-5.65
			LT	0.05960		2.68
NT $\mu = 1.25$			0.05962	0.052	14.65	
Imani Yengejeh et al. (2014)	(5, 5)	15	LEB	0.014	0.012	14.29
			FEM	0.013		7.69
	(10, 10)	15	LEB	0.026	0.026	0
			FEM	0.027		3.7
Lü et al. (2007)	(8, 8)	12.7	MMSMM	0.029	0.03	-3.45

* MD: Molecular Dynamics, LT: Local Timoshenko beam, NT: Nonlocal Timoshenko beam, μ : nonlocal parameter, LEB: Local Euler–Bernoulli beam, FEM: Finite Element Method, MMSMM: Modified Molecular Structural Mechanics Tables may have a footer.

ported beam are given in the graphic form. Five different values of nonlocal parameter were used and its influence on the computed eigenfrequencies is shown.

It can be stated that:

- The effect of the chirality of SWCNTs can be neglected.
- The nanotube eigenfrequencies depend on nonlocal parameters, as well as on the length and diameter of CNTs.
- Increase in the diameter of a carbon nanotube leads to higher eigenfrequencies and the eigenfrequencies of ten times longer carbon nanotubes are hundred times lower.
- Higher nonlocal parameter leads to the smaller eigenfrequencies of CNTs. Ten times higher value of nonlocal parameter leads to approximately three times smaller eigenfrequencies.

- The eigenfrequencies of shorter and, in general, smaller carbon nanotubes are more affected by the value of nonlocal parameter.
- The presented results are in good agreement with the results published in other papers.
- The experimentally measured eigenfrequencies can be used for the determination of Young’s modulus of homogenized single-walled carbon nanotubes.
- In the future work, the finite element method for modeling carbon nanotubes and the effects of boundary conditions, nonlocal parameters and vacancies on mechanical parameters will be investigated.

Data availability. Data can be made available upon reasonable request. Please contact Pavol Lengvarský (pavol.lengvarsky@tuke.sk).

Author contributions. BJ formulated theoretical description of work and prepared analytical formulations; LP performed semi-analytical computations; HR accomplished FEM computations; ŠJ wrote the paper with contributions from all co-authors.

Competing interests. The authors declare that they have no conflict of interest.

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